

Mechanical Design, Instrumentation and Measurements from a Hemoacoustic Cardiac Phantom

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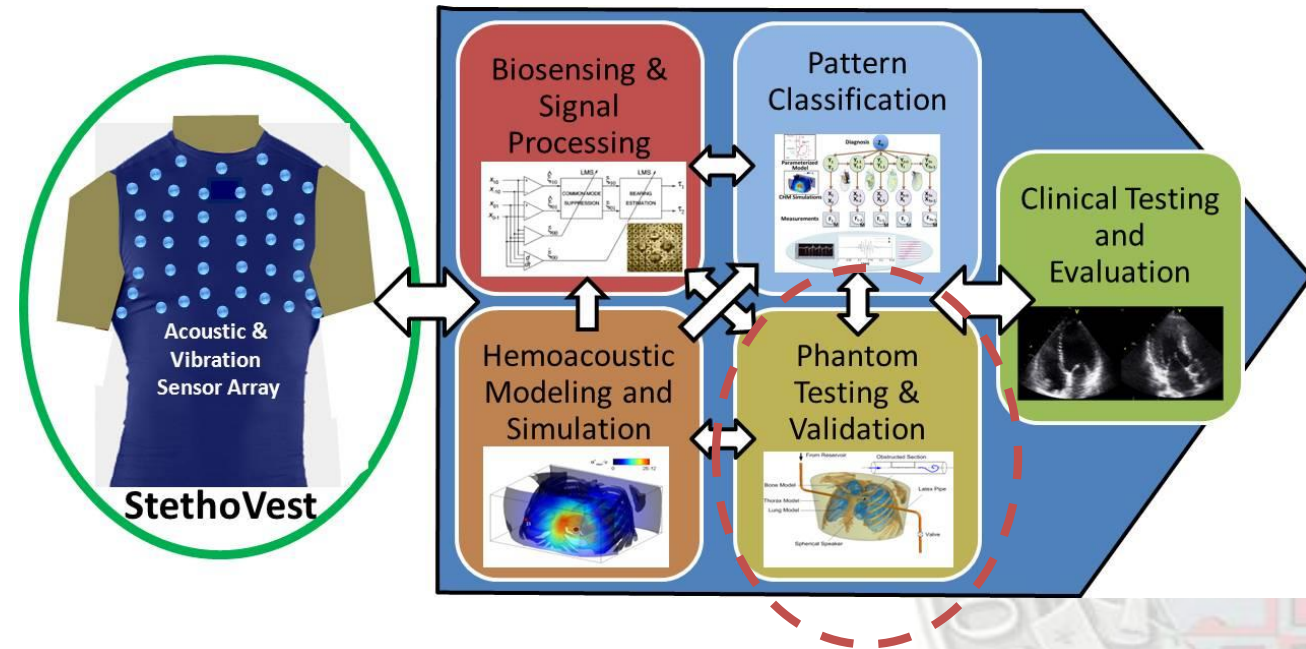
Outline

- Brief overview
- Phantom design
- Hemoacoustic computational simulations
- Comparison between experimental and computational results
- Future versions of the phantom



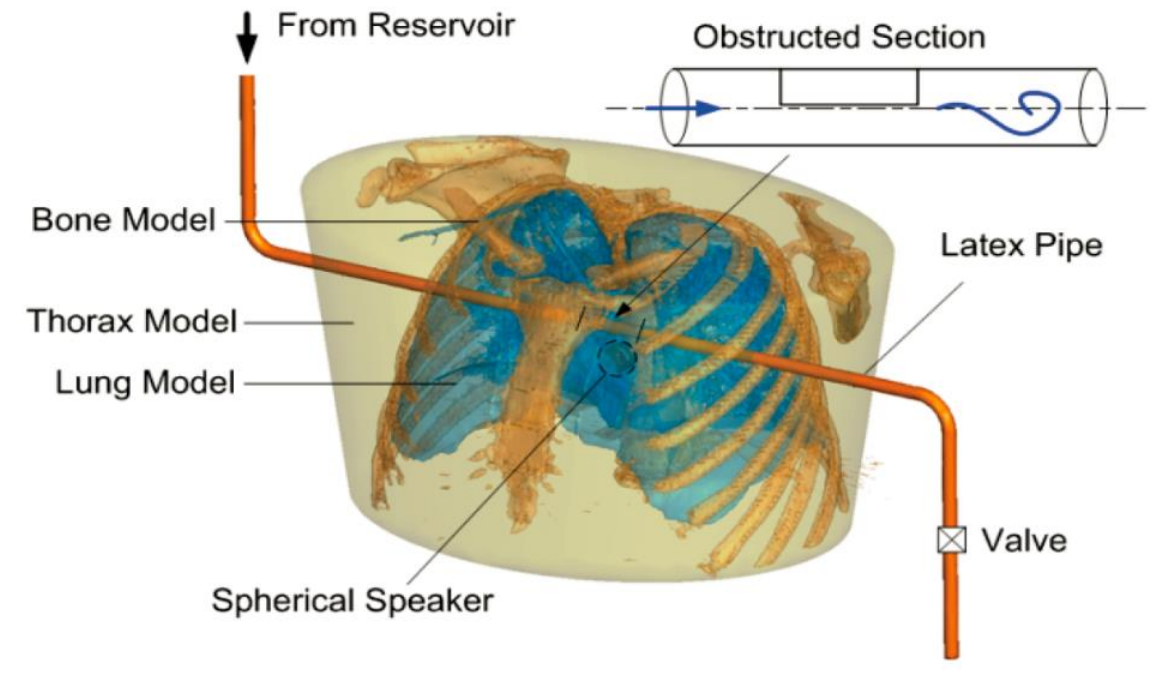
Overview

- **Heart disease:**
 - Most consequential disease in the industrialized world
 - Annual US expenditure on heart disease exceeds half a trillion dollars
- **Cardiac auscultation:**
 - Been around for 200 years
 - Limitations: subjective, inaccurate
- Automated cardiac auscultation via a wearable acoustic array (the "StethoVest"):
 - Expensive → Cost-effective
 - Reactive → Proactive,
 - Hospital centric → Patient centric



Developing the thoracic phantom

- The phantom will be used to validate the codes and to examine the sensors
- To design the phantom the following items should be considered :
 - Tissue mimicking homogeneous material and characterization
 - Murmur generating embedded fluid-circuit
 - Measurements : Variety of acoustic sensors



Material selection

- Acoustic and mechanical properties should be similar
- Examples of previous tissue-mimicking materials in the literature
 - Agar
 - Silicone
 - Polyvinyl alcohol gel (PVA) and
 - Polyacrylamide gel (PAA)



Acoustic property of the material

Table 2. Sound velocities, densities, impedances, and acoustic attenuation coefficients of silicone, agar, PVA and PAA in comparison to the values of human tissues and literature values.

Material	Velocity, c_s (10^3 m s^{-1})	Density, ρ (10^3 kg m^{-3})	Impedance z ($10^6 \text{ kg m}^{-2} \text{ s}^{-1}$)	Acoustic attenuation coefficient, α (dB cm^{-1})	Frequency (MHz)	References
Human breast tissue	1.43–1.57	0.99–1.06	1.42–1.66 ^b	9.5 –12.6	7	Duck 1990
Human skin	1.54 ^a	1.11–1.19	1.71–1.83 ^b	9.2 + 2.2	5	Duck 1990
Silicone	1.03 ± 0.06 ^c	1.07 ± 0.03	1.10 ± 0.05 ^c	14.0 ± 1.4	5	our measurement
				14.7 ± 1.6	7	
PVA	1.57 ± 0.02 ^c	1.10 ± 0.05	1.74 ± 0.08 ^c	2.9 ± 0.1	5	our measurement
				3.2 ± 0.1	7	
	1.58 ± 0.03	1.07 ± 0.02	1.71 ± 0.06	2.1	5	Kharine <i>et al</i> 2003
PAA (10%)	1.58 ± 0.05 ^c	1.09 ± 0.09	1.73 ± 0.08 ^c	0.7 ± 0.1	5	our measurement
				0.7 ± 0.1	7	
	–	1.02 ± 0.01	–	0.4 ± 0.1	5	Prokop <i>et al</i> 2003
Agar 2%	1.50 ± 0.03 ^c	1.04 ± 0.11	1.57 ± 0.08 ^c	0.4 ± 0.1	5	our measurement
				0.5 ± 0.1	7	
	1.54	–	–	–	–	Browne <i>et al</i> 2003

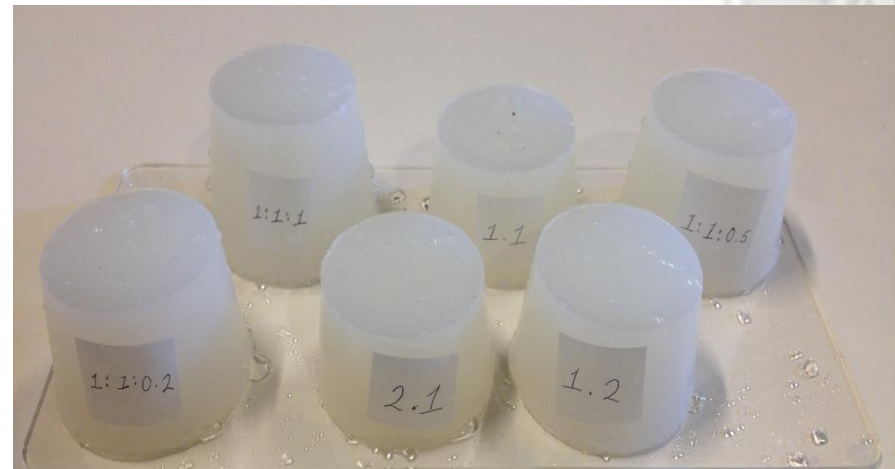
Mechanical Property

Table 1. Soft materials used in the study.

No.	Material, manufacturer, city, state	Density (g ml ⁻¹)	Softener volume range ^a (%)	Modulus range ^a (kPa)	Approximate cost per gallon
1	SR-1610, Douglas and Sturgess, San Francisco, CA	1.15	0–58 ^b	25–660	\$100
2	Dragon skin, Smooth-On, Easton, PA	1.08	0–78 ^b	20–850	\$85
3	Ecoflex 00-10, Smooth-On, Easton, PA	1.03	0–50 ^b	15–110	\$105
4	HS-IV, Dow Corning, Midland, MI	1.11	0–48 ^b	20–570	\$140
5	Candle Gel, Endless Possibilities, Oklahoma City, OK	0.98	n/a	50	\$35
6	Tin-Sil, US Composites, West Palm Beach, FL	1.07	0–82 ^b	10–1400	\$200
7	Semicosil 921, Wacker Solutions, Adrian, MI	1.10	n/a	25	\$110
8	8116SS plastic, M-F Manufacturing, Ft. Worth, TX	0.99	0–56 ^c	15–200	\$40
9	CF11, Nusil Technologies, Carpinteria, CA	1.04	n/a	204	\$240

Silicone rubber

- Silicone rubber, Ecoflex 010 (Smooth-on)
 - Easy to produce ,
 - extremely stable
 - non-toxic and
 - negligible shrinkage
- Procedure to make :
 - Mixing Part A part B,
 - Adding Silicon thinner,
 - Degassing for 3-4 min in (-29 in Hg) to remove air bubbles

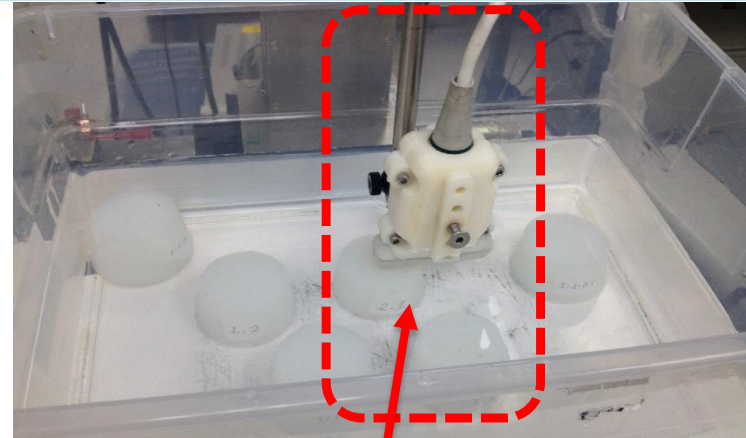
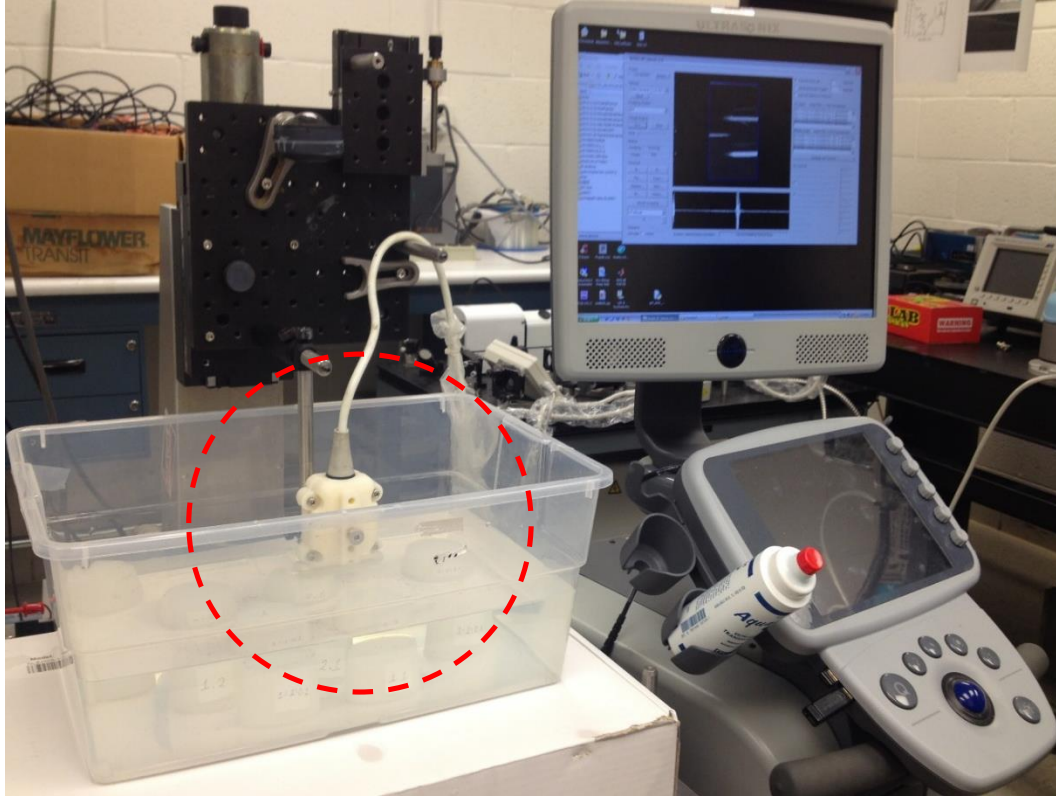


Material characterization

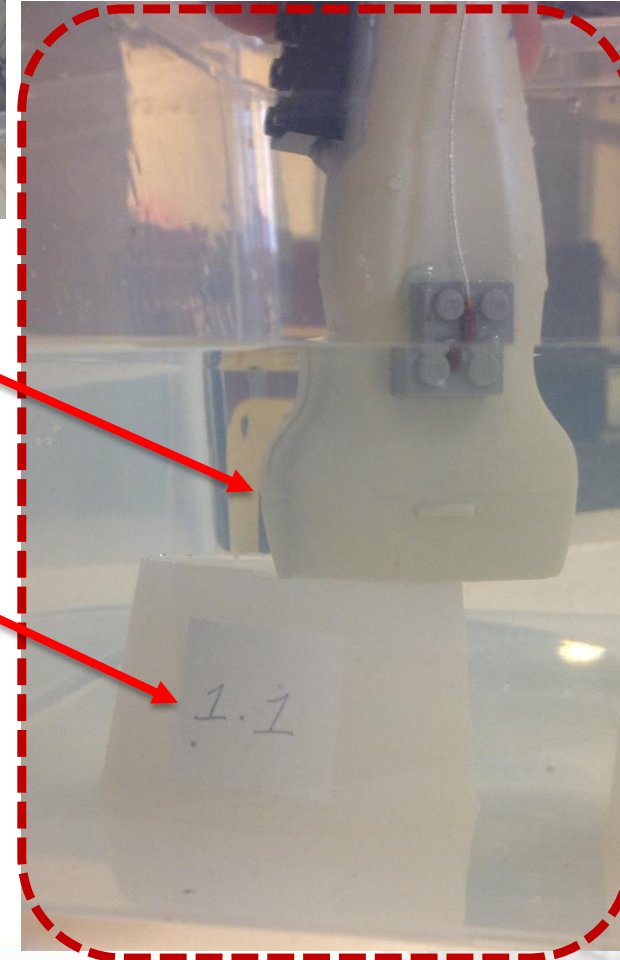


Speed of sound

Speed of sound : 993-1043m/s



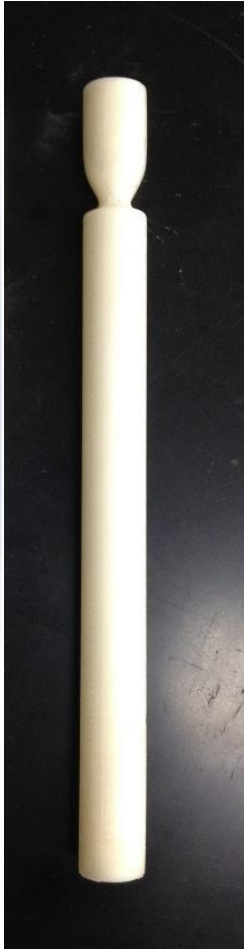
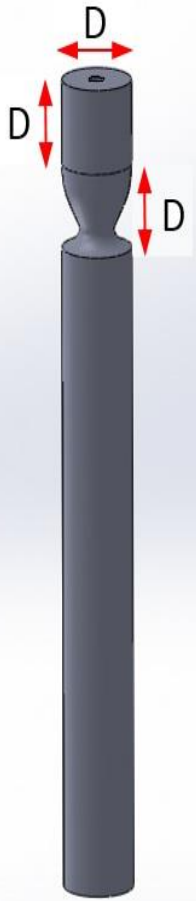
Ultrasound Probe



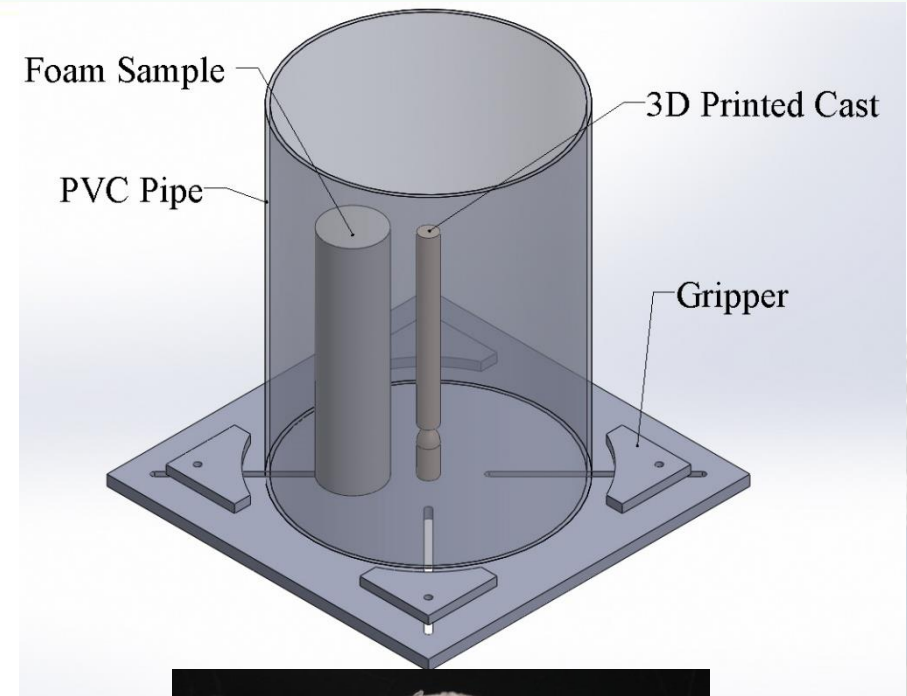
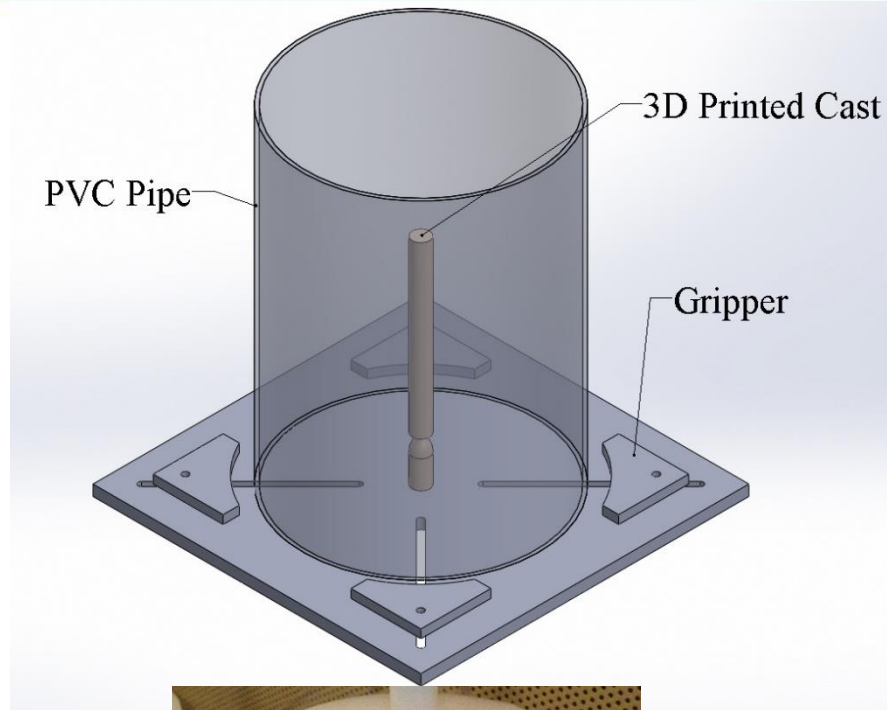
Gel sample

The ratio of sound speeds are equal to the inverse ratio of the depth seen in the ultrasound image

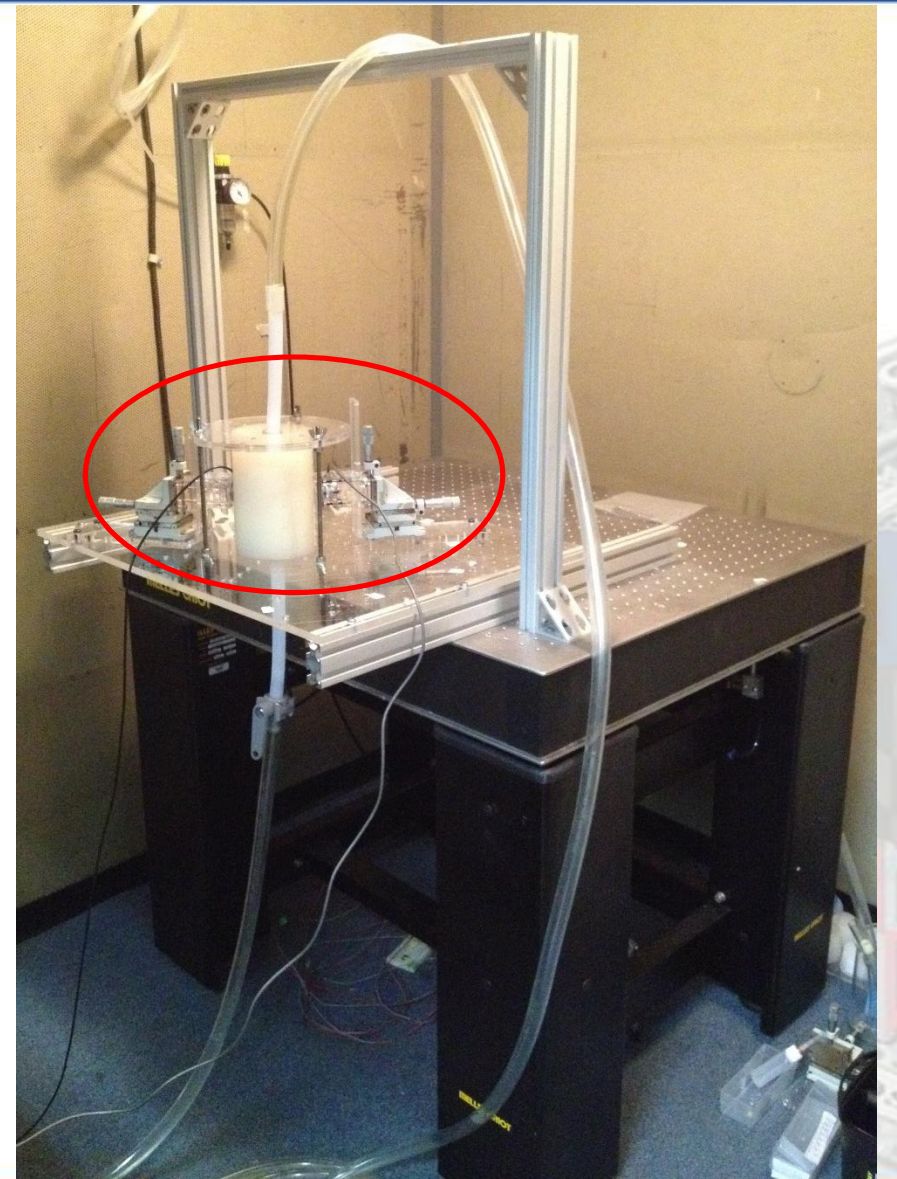
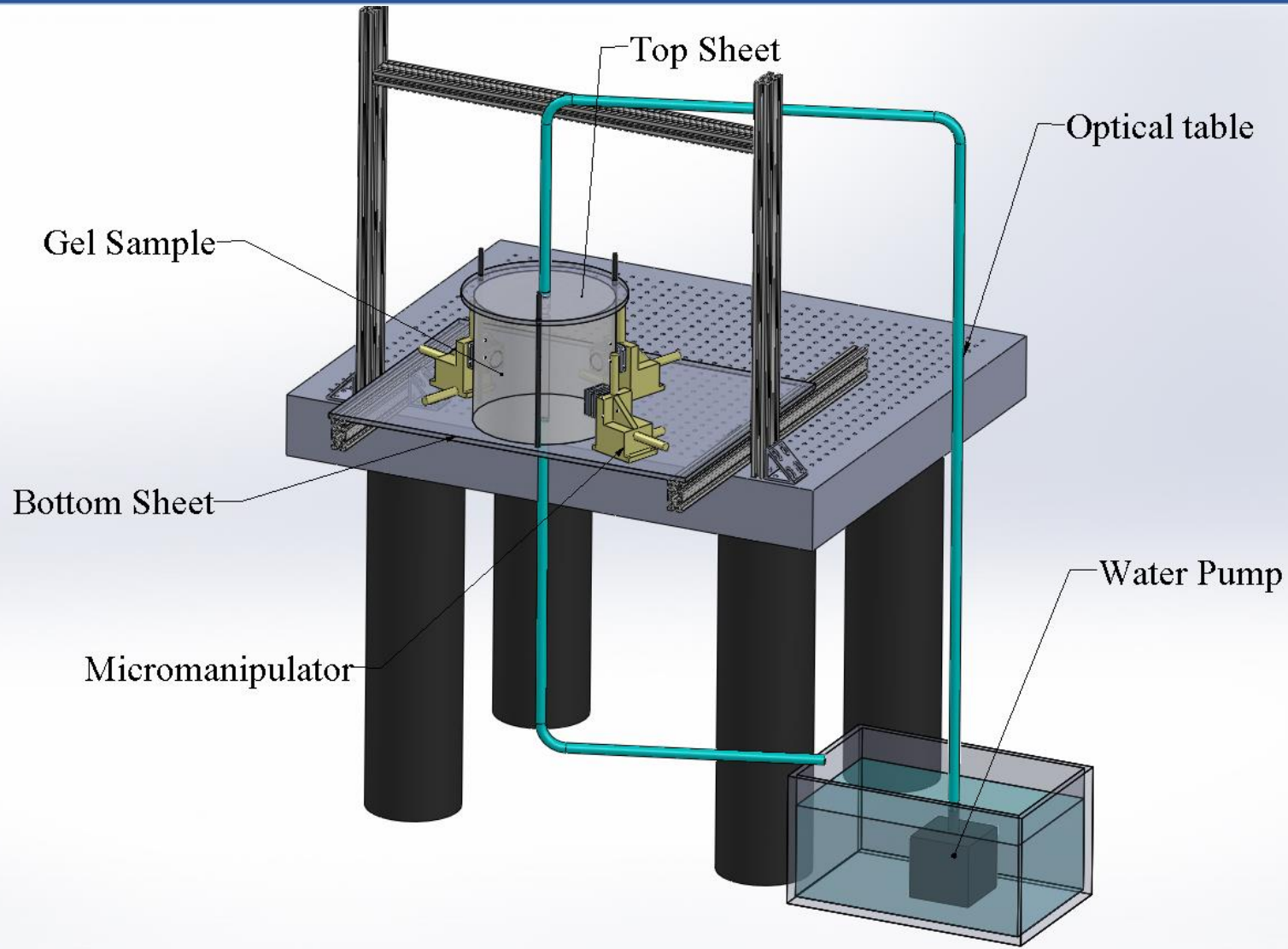
Murmur generating



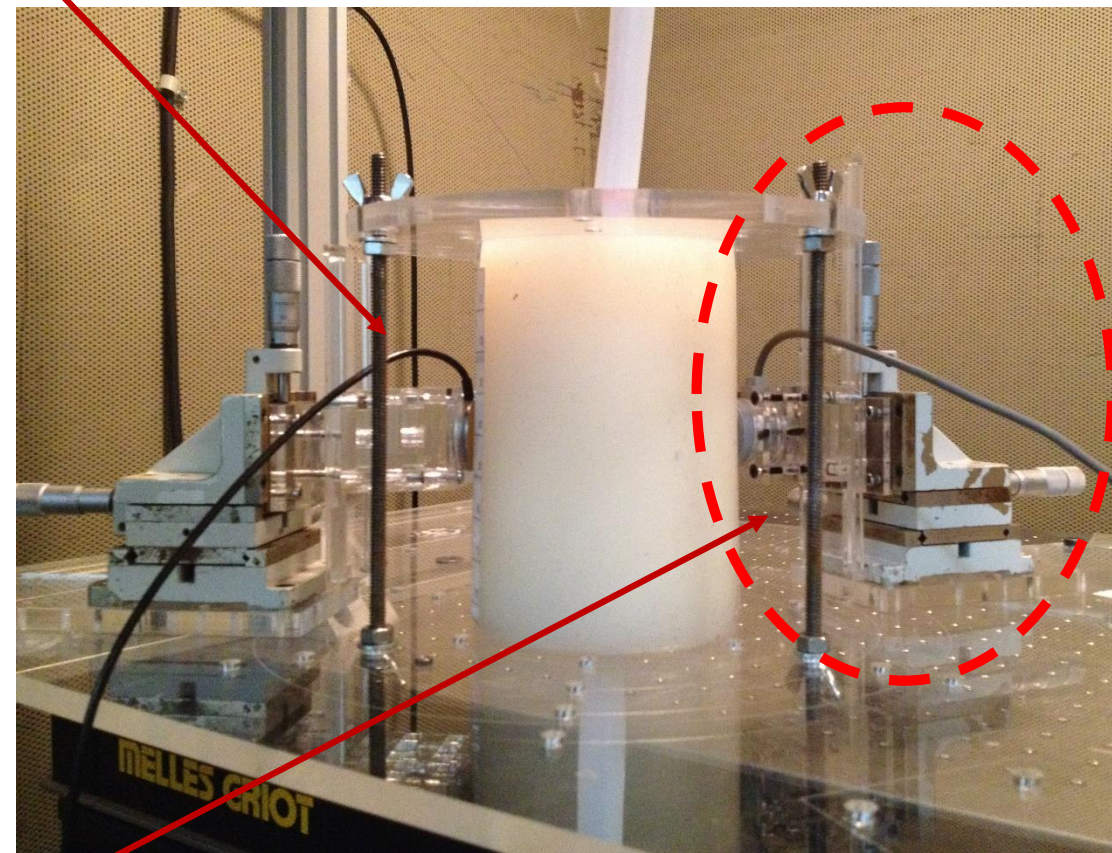
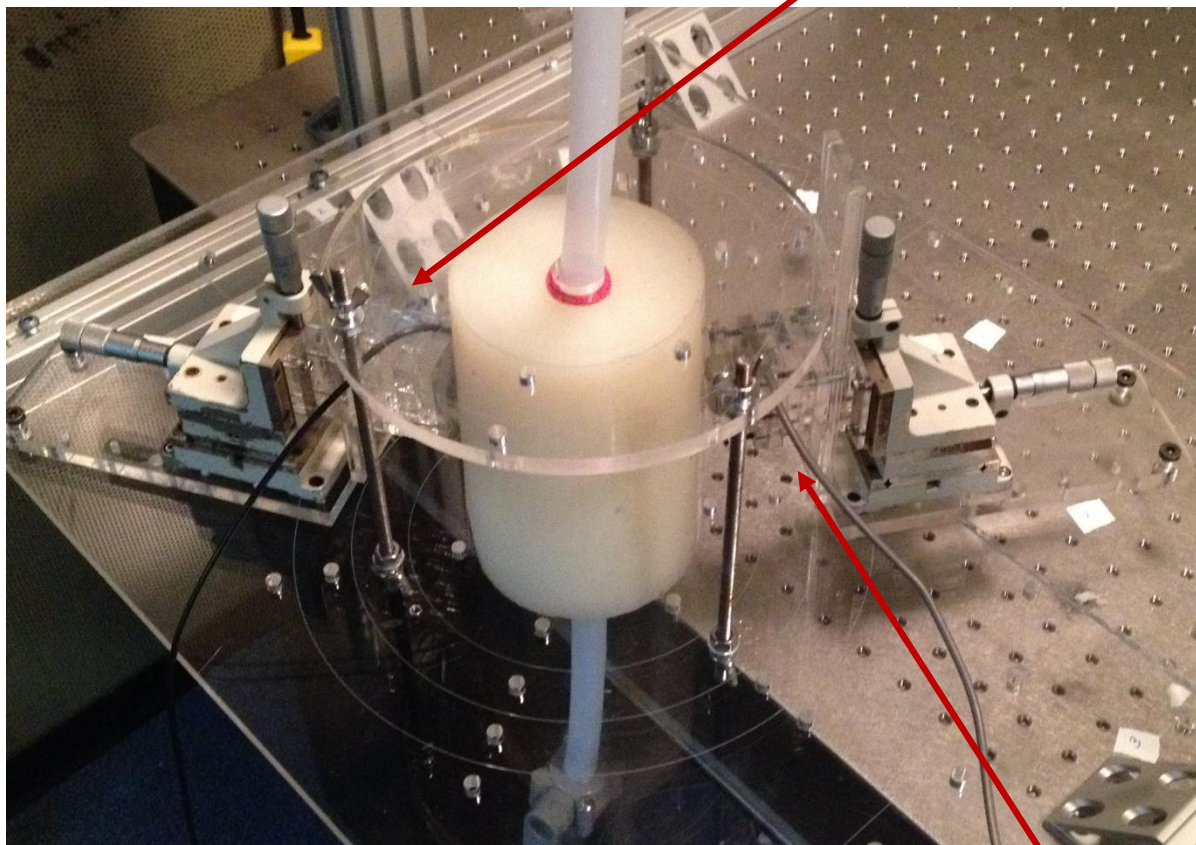
3D printed Cast



Fluid Flow Circuit

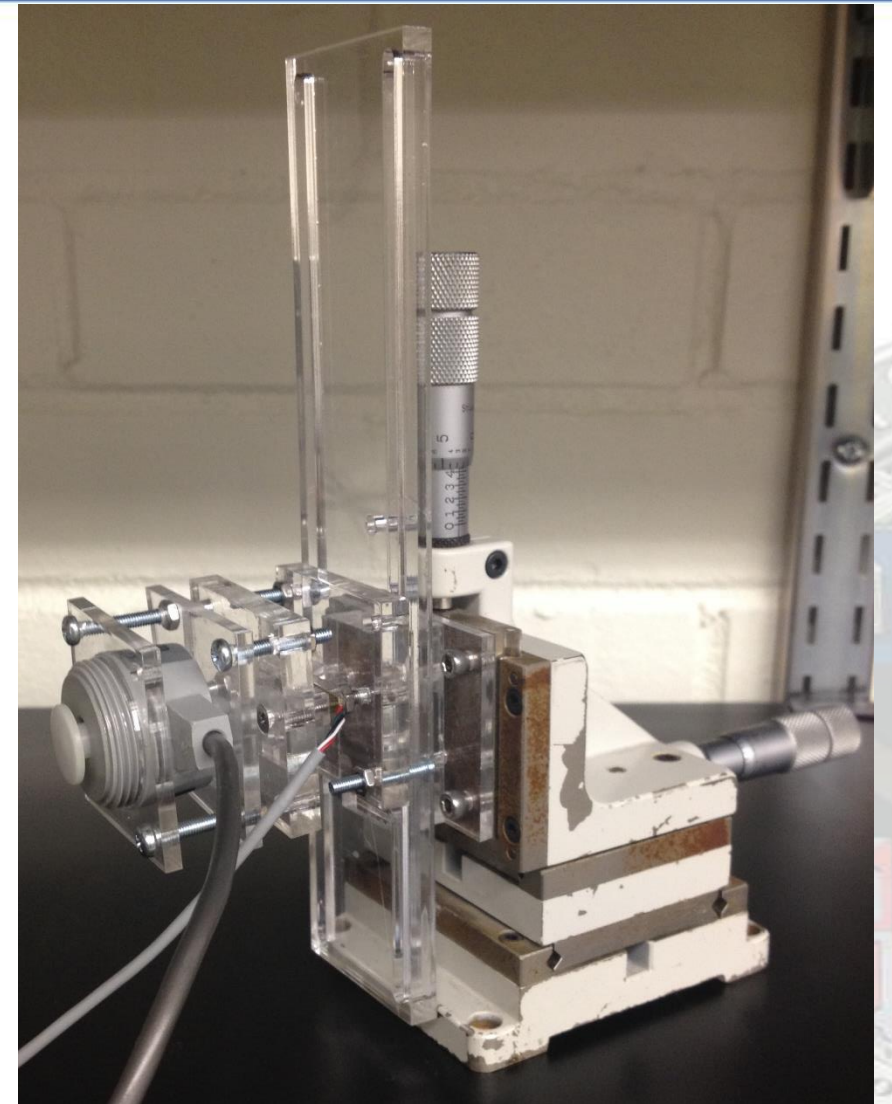
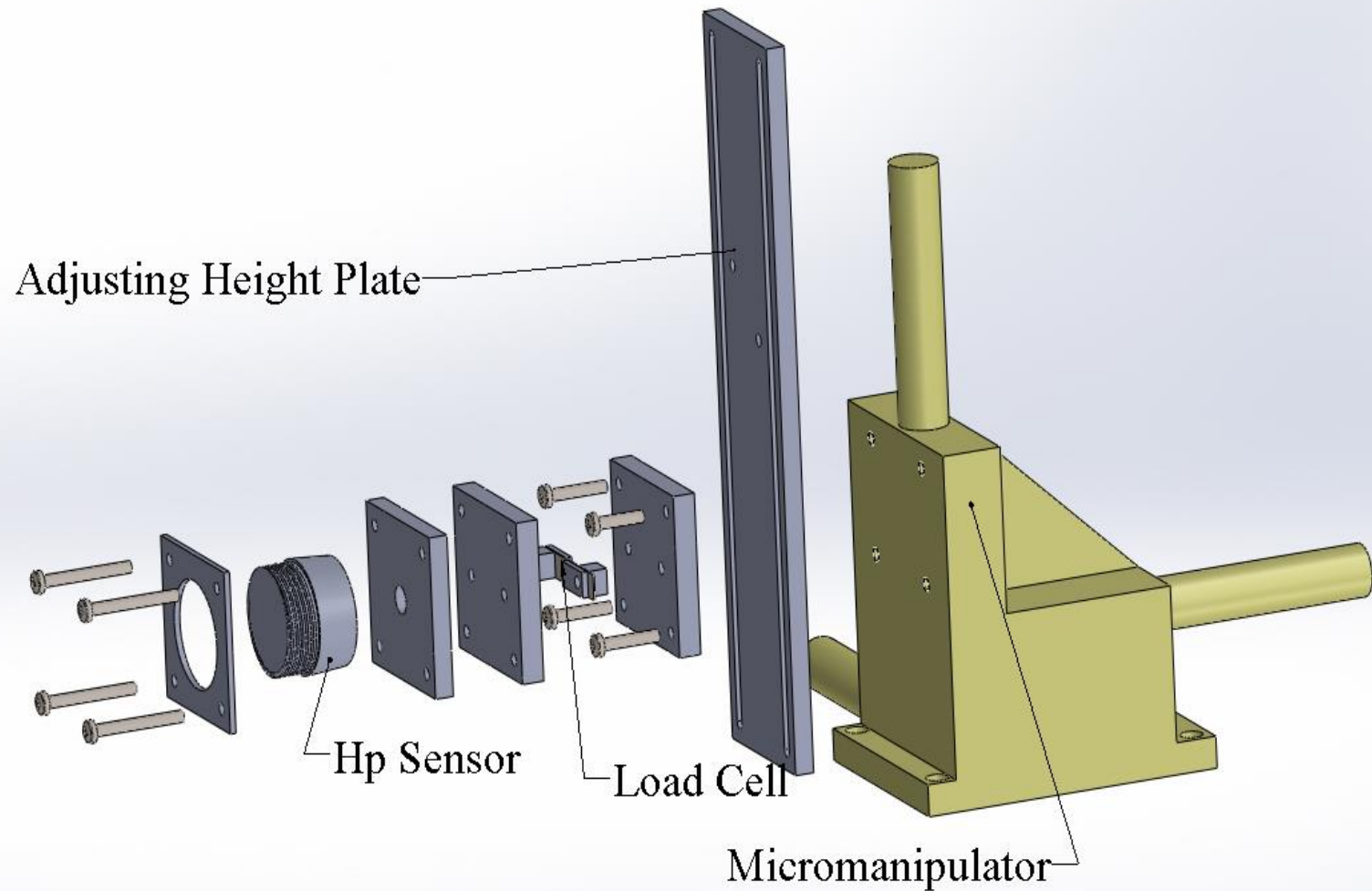


Bipac sensor attached to the Micromanipulaor



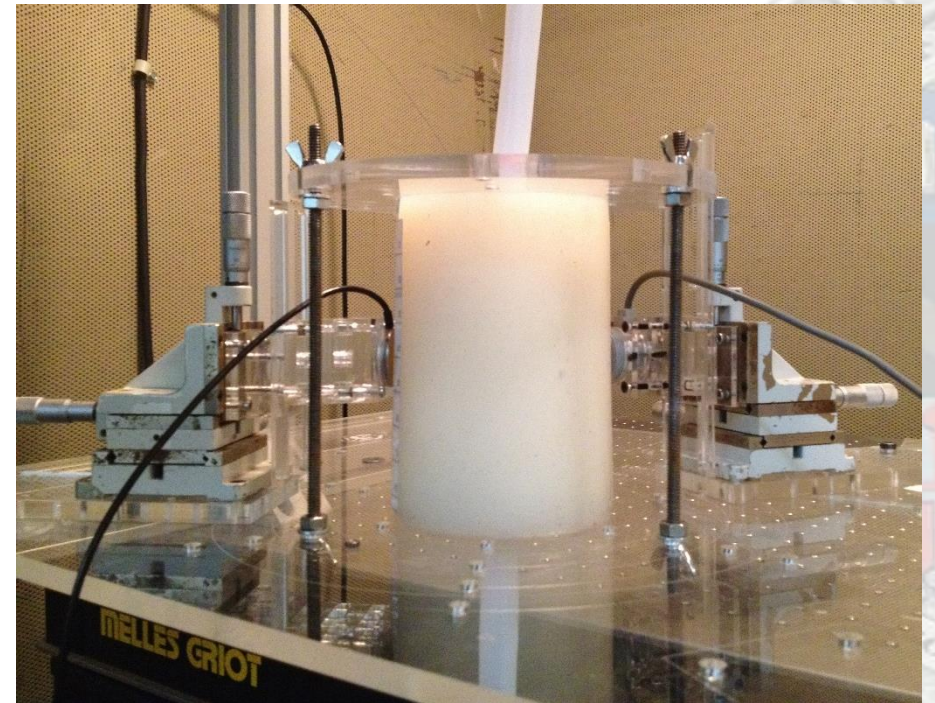
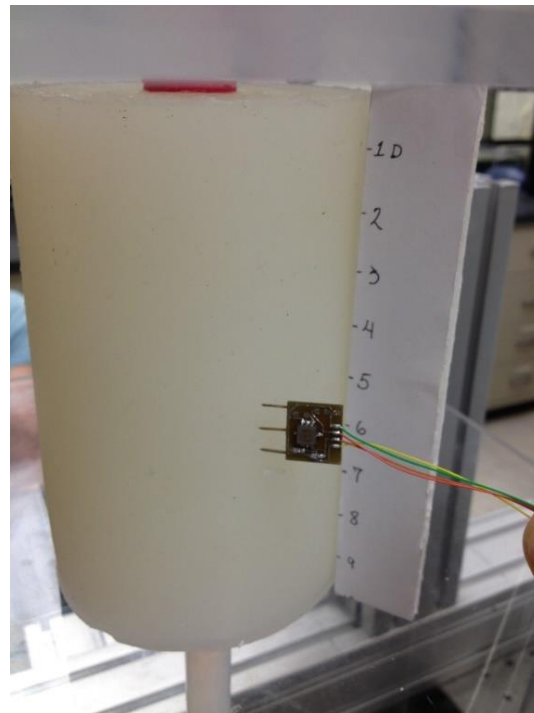
HP sensor attached to the Micromanipulaor

Micromanipulators



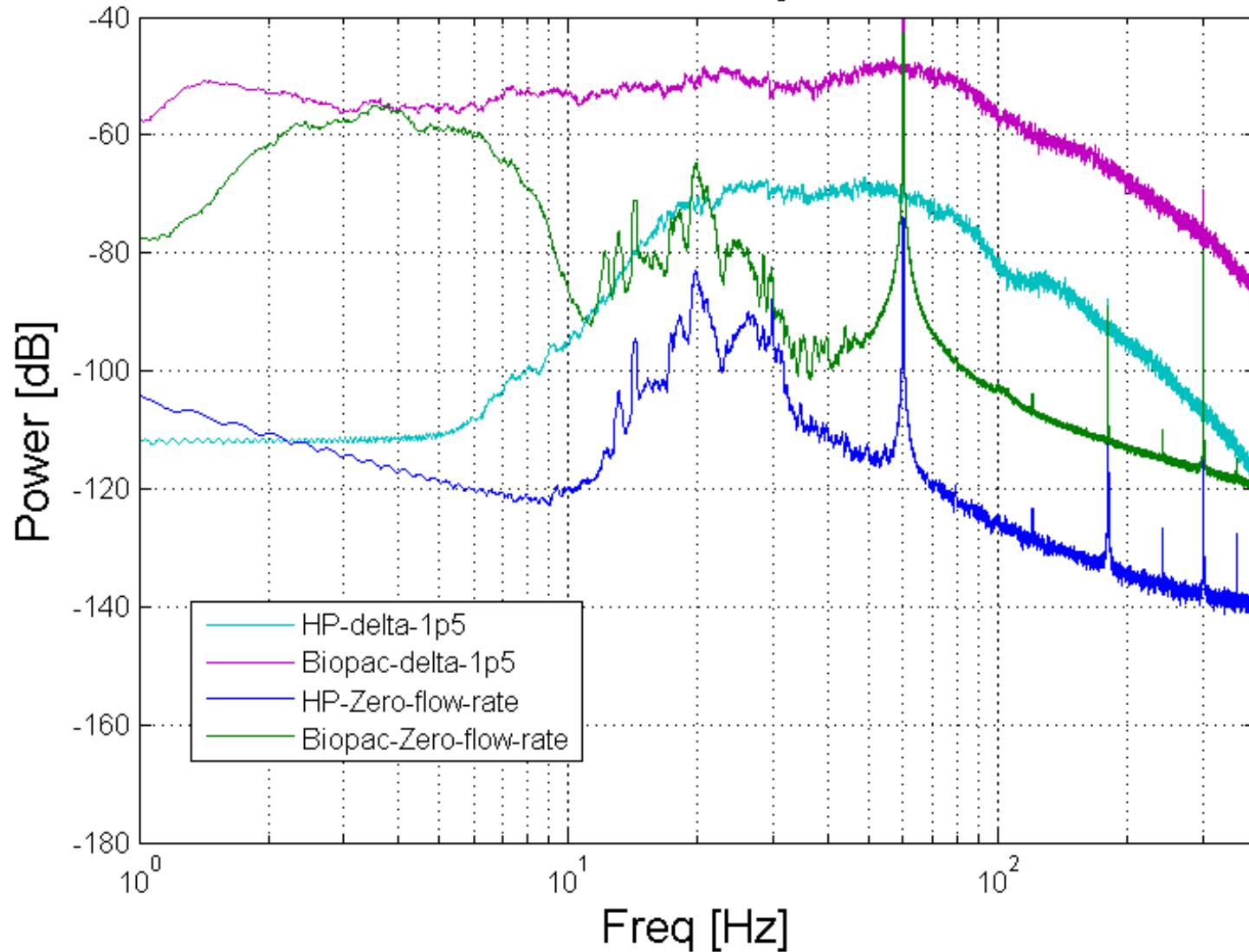
Measurements

- Different acoustic sensors used in the phantom tests.
 - A: Commercially available electronic stethoscope.
 - B: Accelerometers
 - C: HP 21050A sensor mounted on a micromanipulator.
 - D: Biopac sensors



Sensor selection ...

HP1 & Biopac

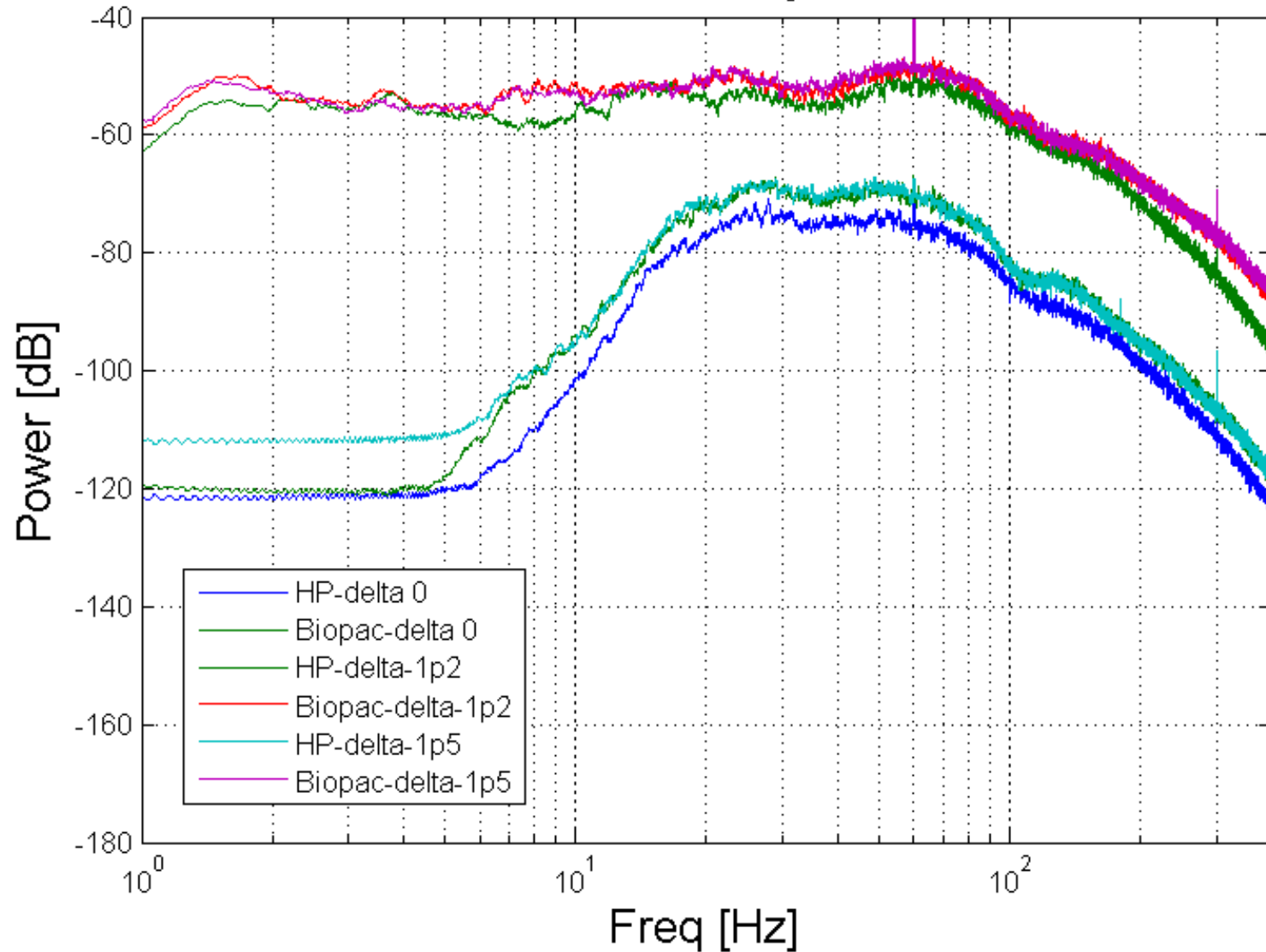


- Pump was turned on and off
- Clear difference between two diagrams for HP and Biopac
- Poor SNR for stethoscope and the accelerometer



Effect of Indentation

HP1 & Biopac



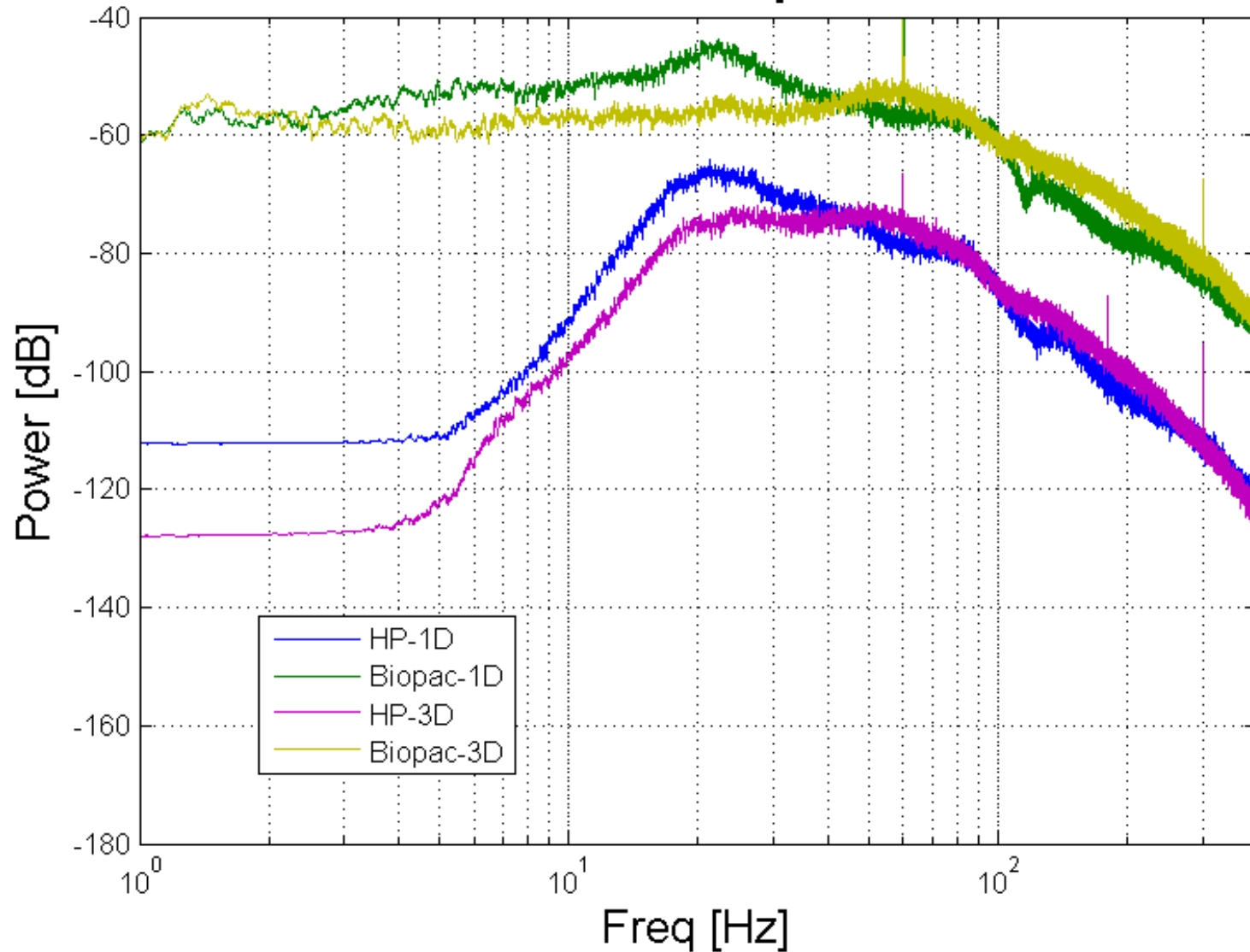
To compare the effect of indentation :

- Reference position :Sensors touching the sample
- Gradual increase in the indentation
- Indentation = 0, 0.03, 0.06, 0.09, 0.12 and 0.15 in $\sim 0 : 0.76 : 3.81$ mm
- After 0.12, no differences were observed



Distance after the constriction

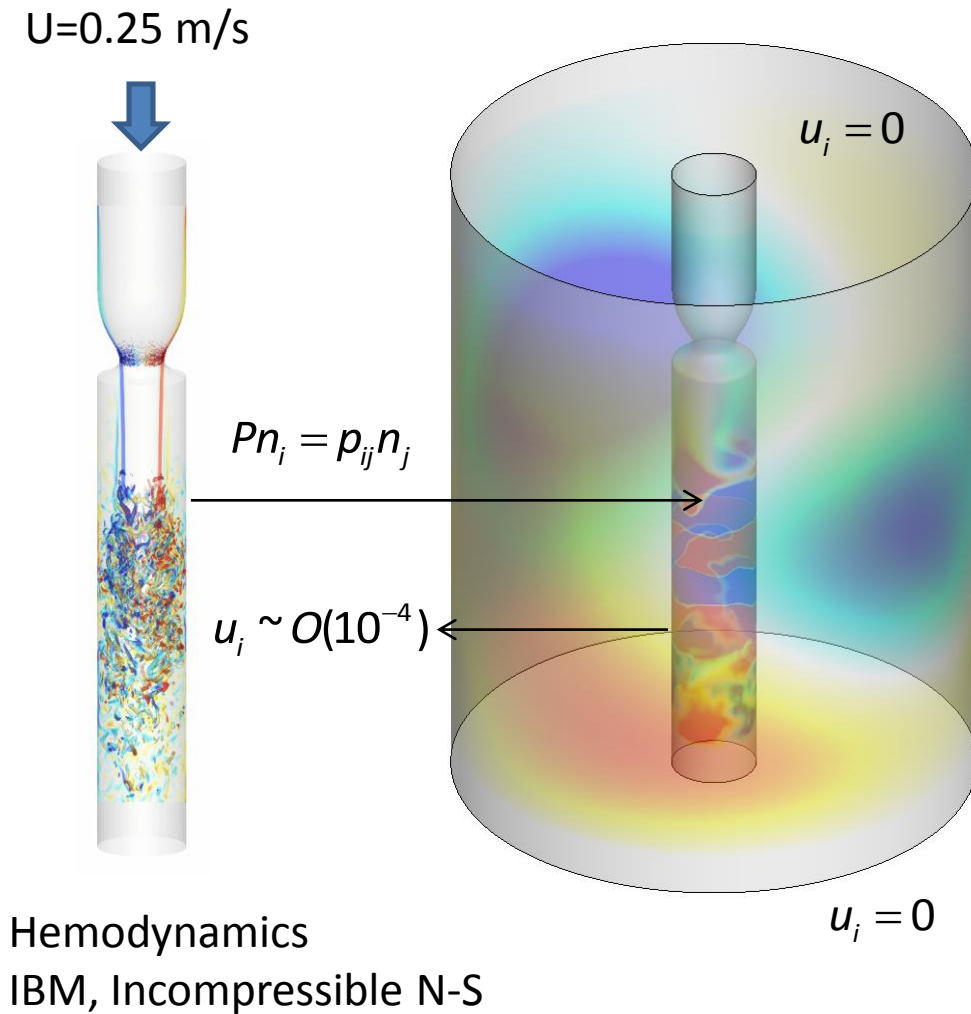
HP1 & Biopac



Computational model

By Dr. Jung-Hee Seo

Hemoacoustic Simulation



Structural wave eq.
For viscoelastic material

Generalized Hooke's law
Kelvin-Voigt model

$$\frac{\partial p_{ij}}{\partial t} + \lambda \frac{\partial u_k}{\partial x_k} \delta_{ij} + \mu \left(\frac{\partial u_i}{\partial x_j} + \frac{\partial u_j}{\partial x_i} \right) = 0$$

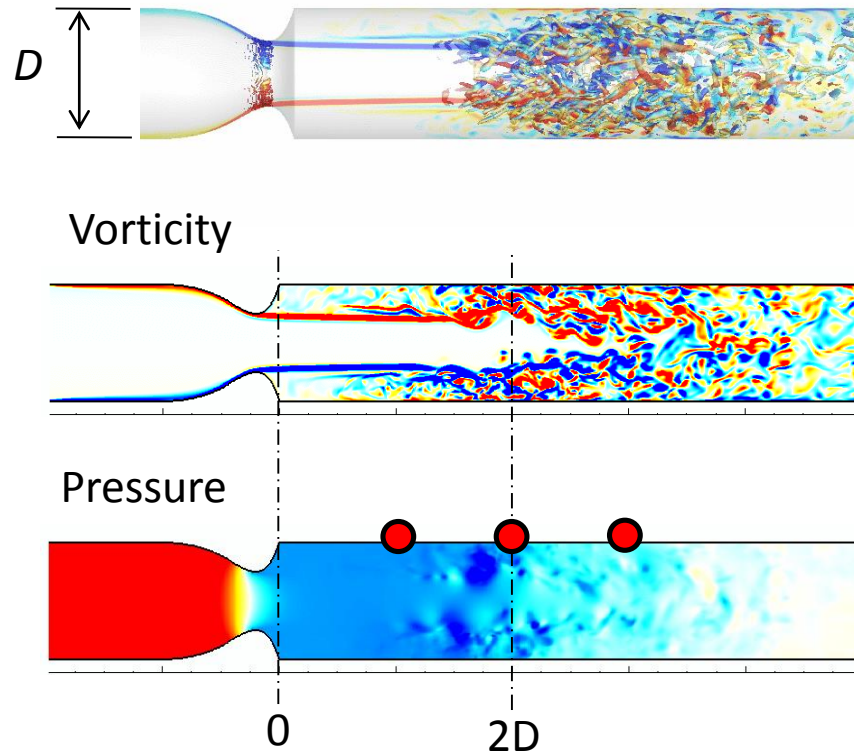
$$\frac{\partial u_i}{\partial t} + \frac{1}{\rho} \frac{\partial p_{ij}}{\partial x_j} = \frac{\eta}{\rho} \frac{\partial}{\partial x_j} \left(\frac{\partial u_i}{\partial x_j} + \frac{\partial u_j}{\partial x_i} \right)$$

High-order IBM,
6th order Compact Finite
Difference Scheme,
4 stage Runge-Kutta method

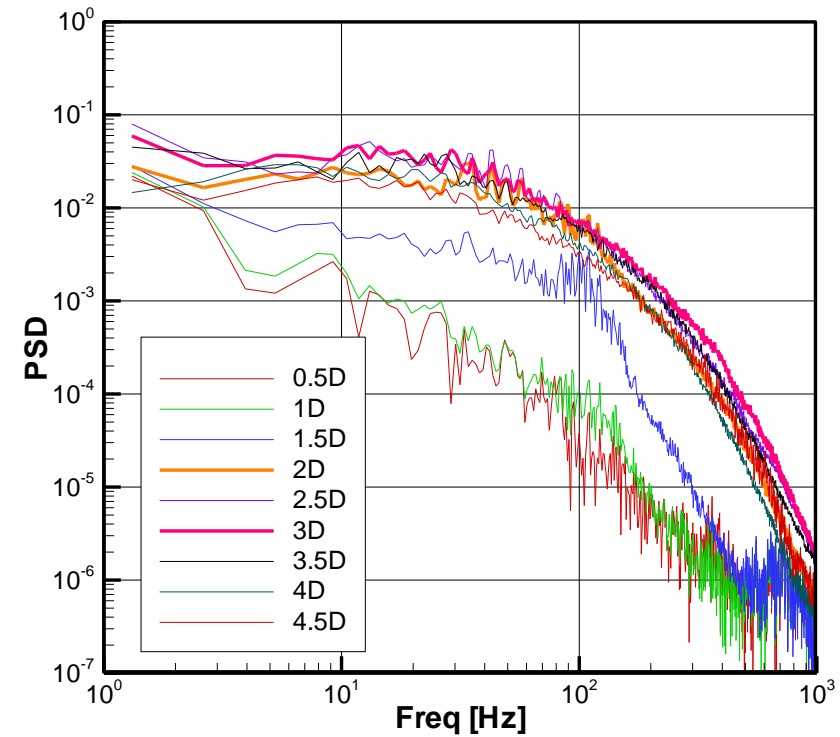
Hemodynamic Simulation Results

3D vortical structure

$Re_D=4000$



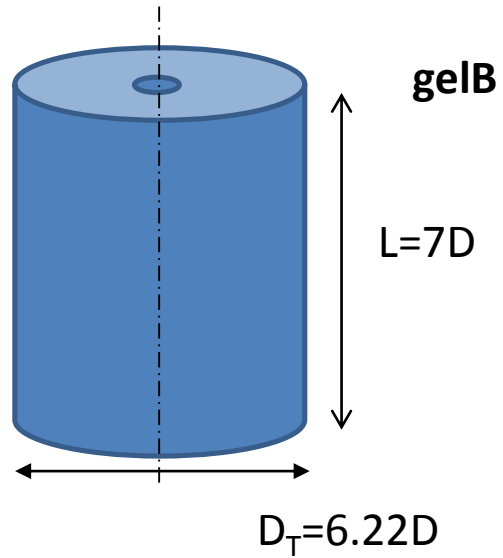
Wall pressure spectrum



Pressure fluctuation is responsible for the murmur generation

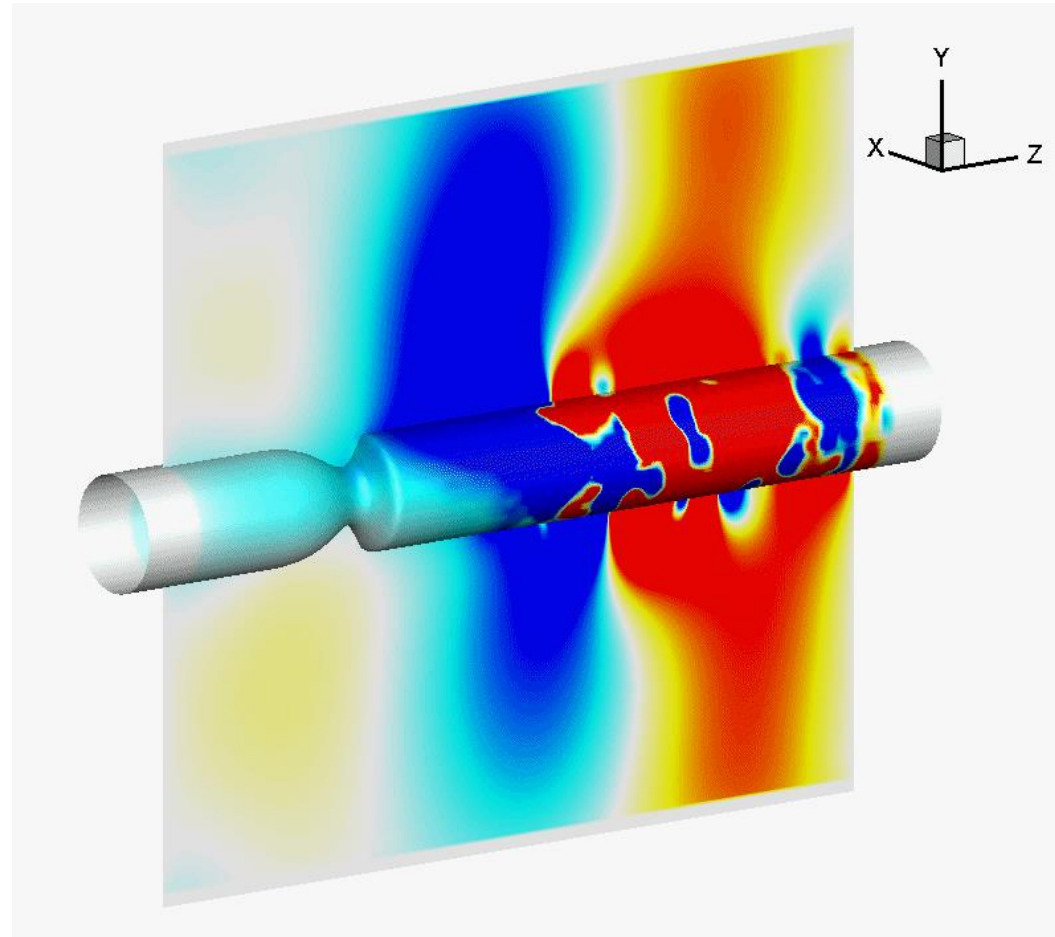
Strong pressure fluctuations are observed beyond 2D downstream of the stenosis

3D Elastic Wave Simulation

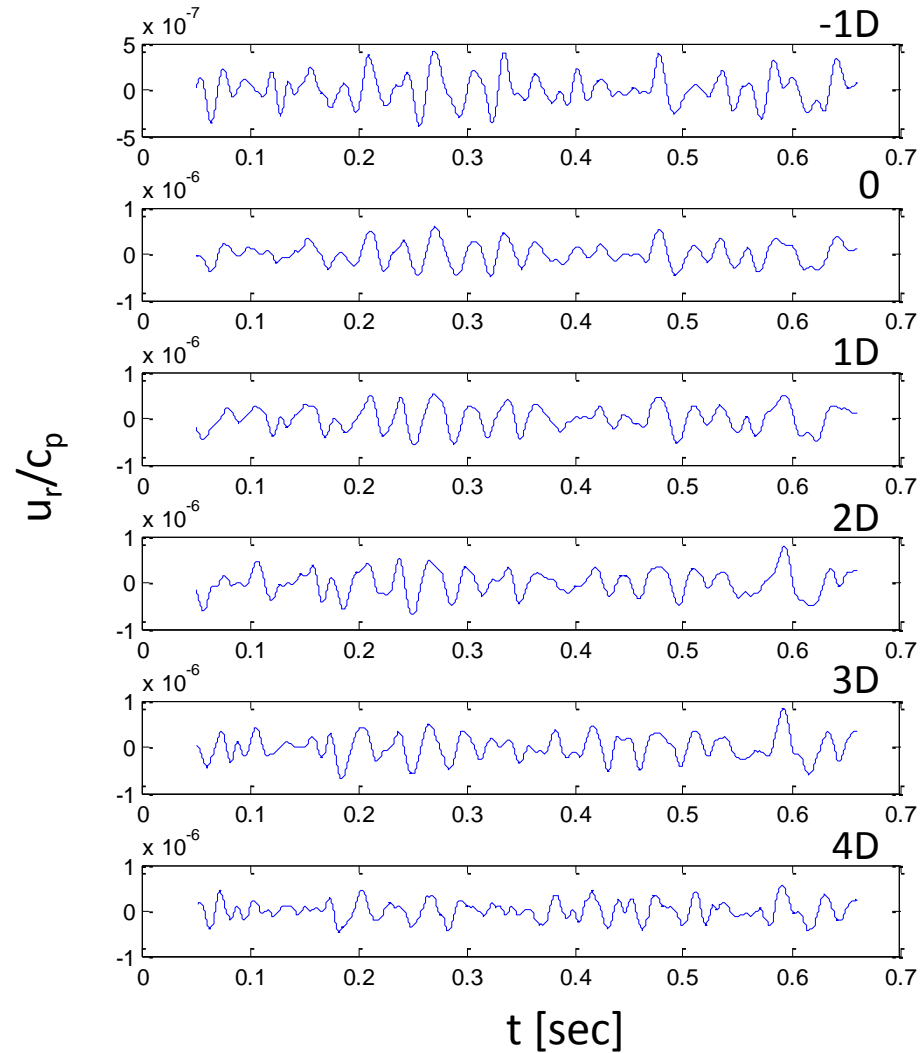
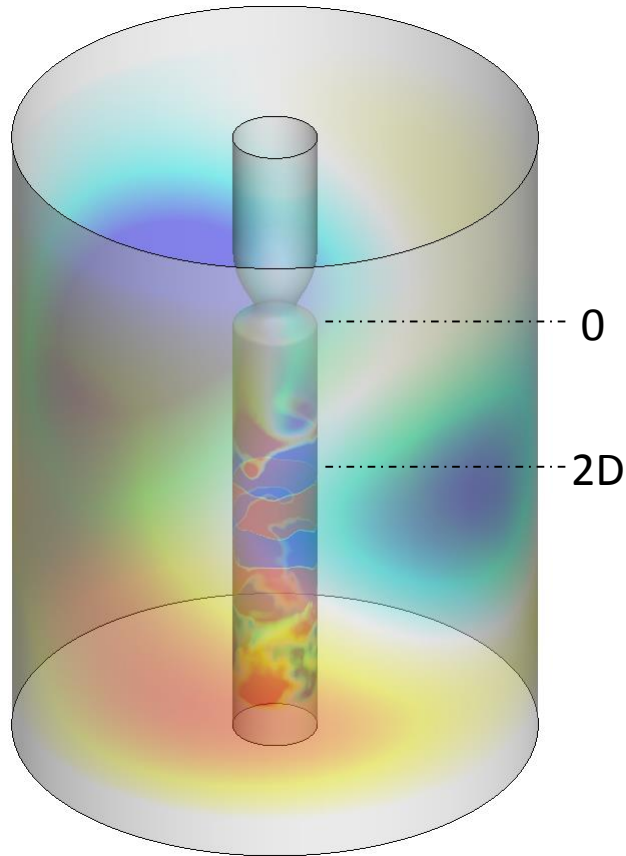


- 200x200x320 (12.8 M)
- Compression wave speed is reduced by an order (100 m/s)
- Shear wave speed remains the same (4.2 m/s)
- 200 hrs with 256 cores for real time 0.8 sec

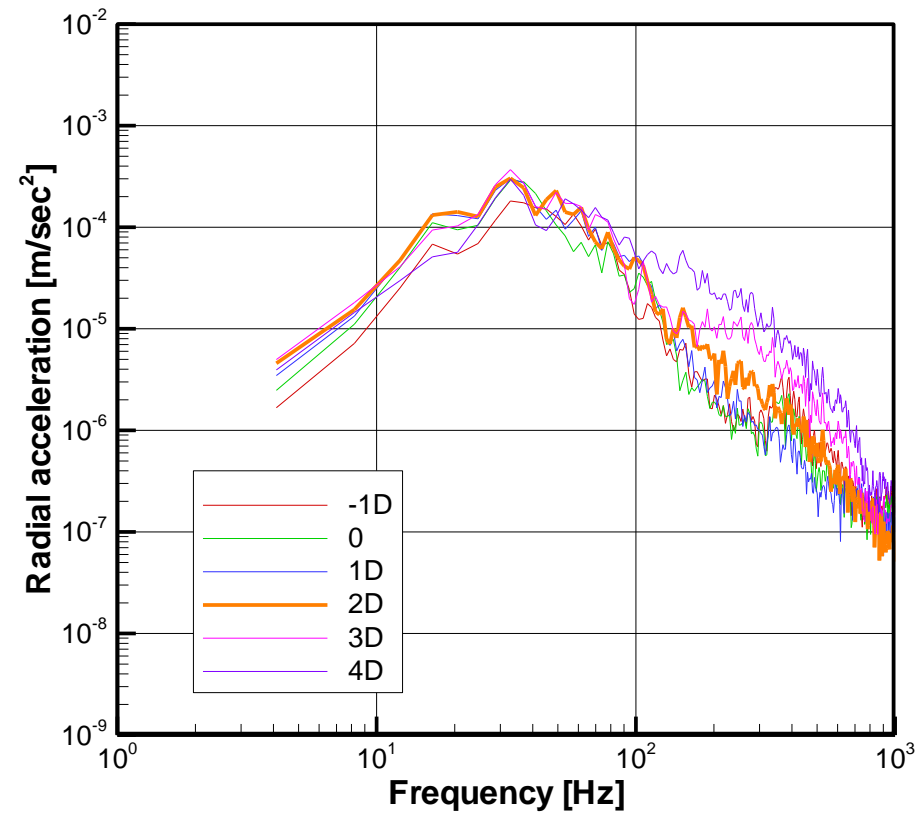
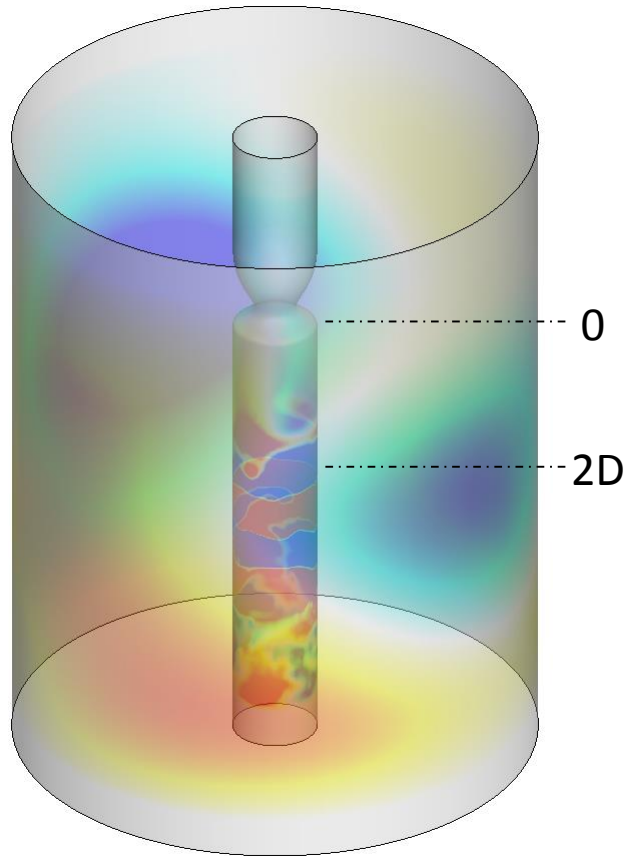
Radial velocity fluctuation



Surface Velocity Fluctuations

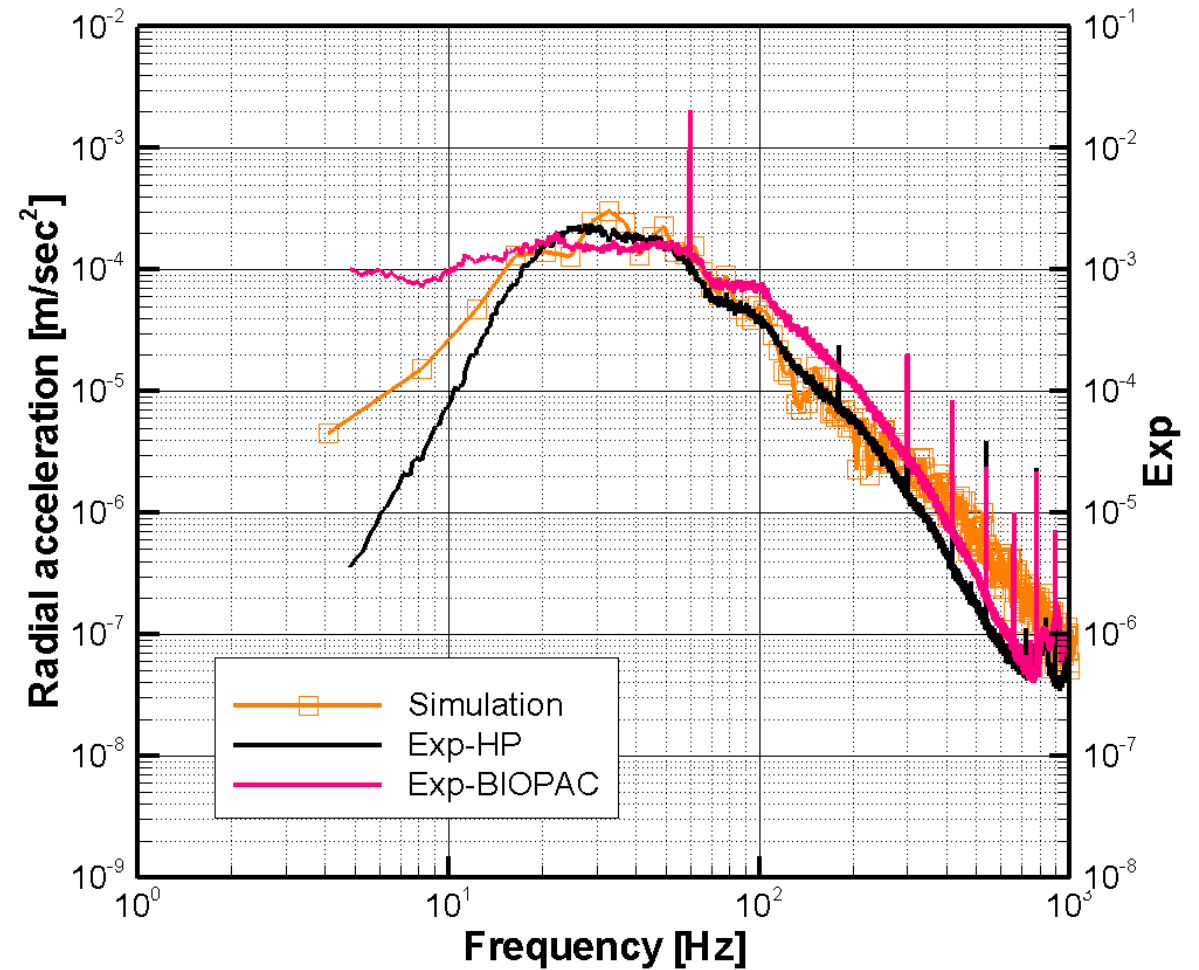


Surface Acceleration Spectrum



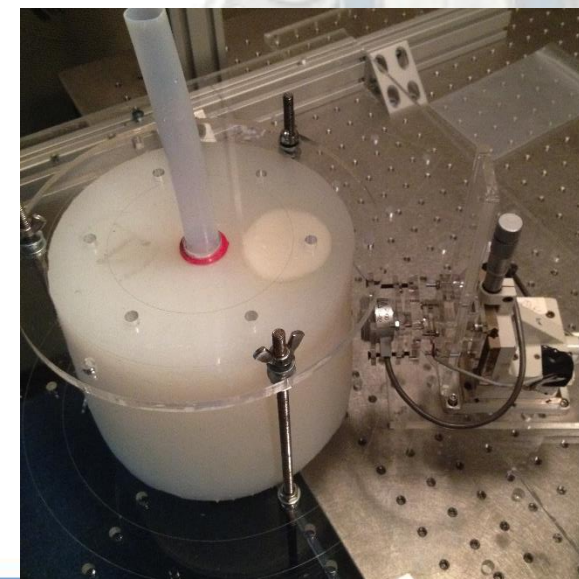
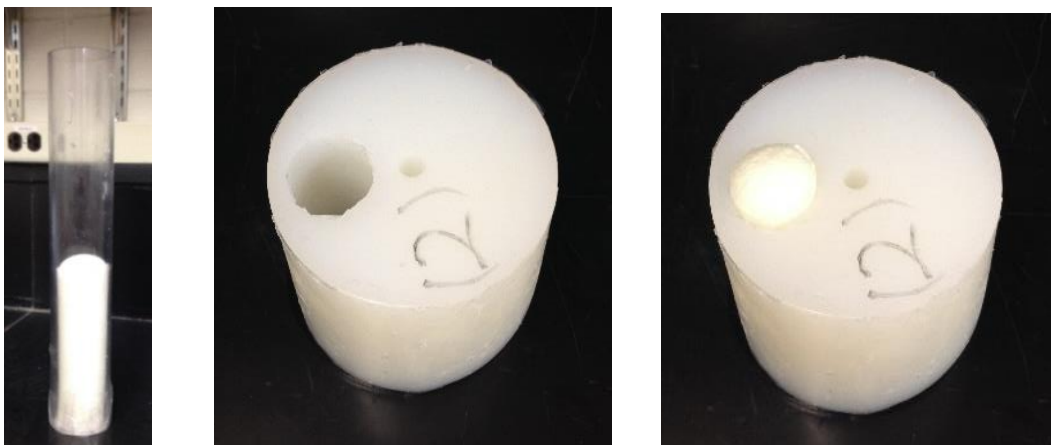
Comparison

- The frequency spectrum of the measured acceleration at the downstream location is plotted along with the computational ones



Future versions

- Adding lung to the phantom
- Foam is used to model the lung
- Non-axisymmetric model



Summary

- Different steps to make the Cardiothoracic phantom were explained
 - Material selection and characterization
 - Murmur generating embedded fluid-circuit
 - Measurements options
- Hemoacoustic simulation results were presented and compared with those from experiment
 - Good agreement was seen based on the preliminary results



Acknowledgment

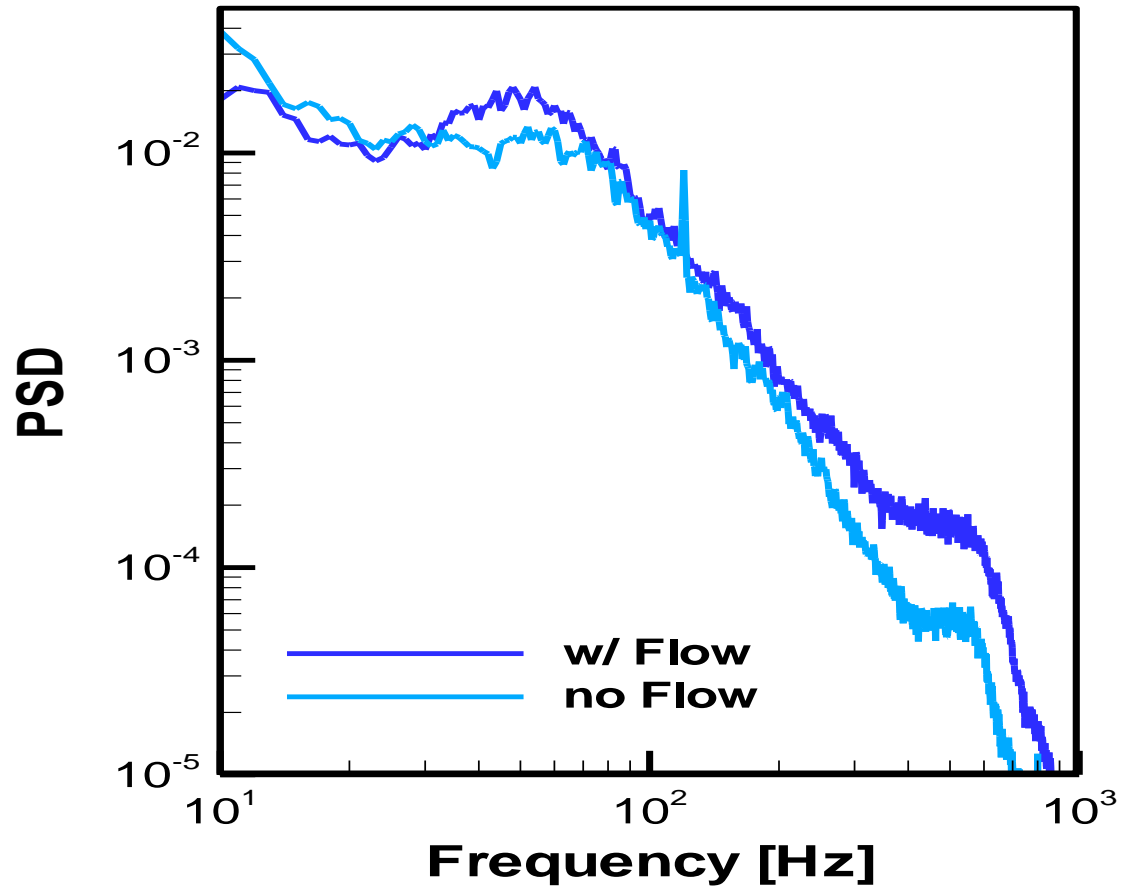
- Dr. Emad Boctor and Fereshteh Alamifar
- NSF for funding



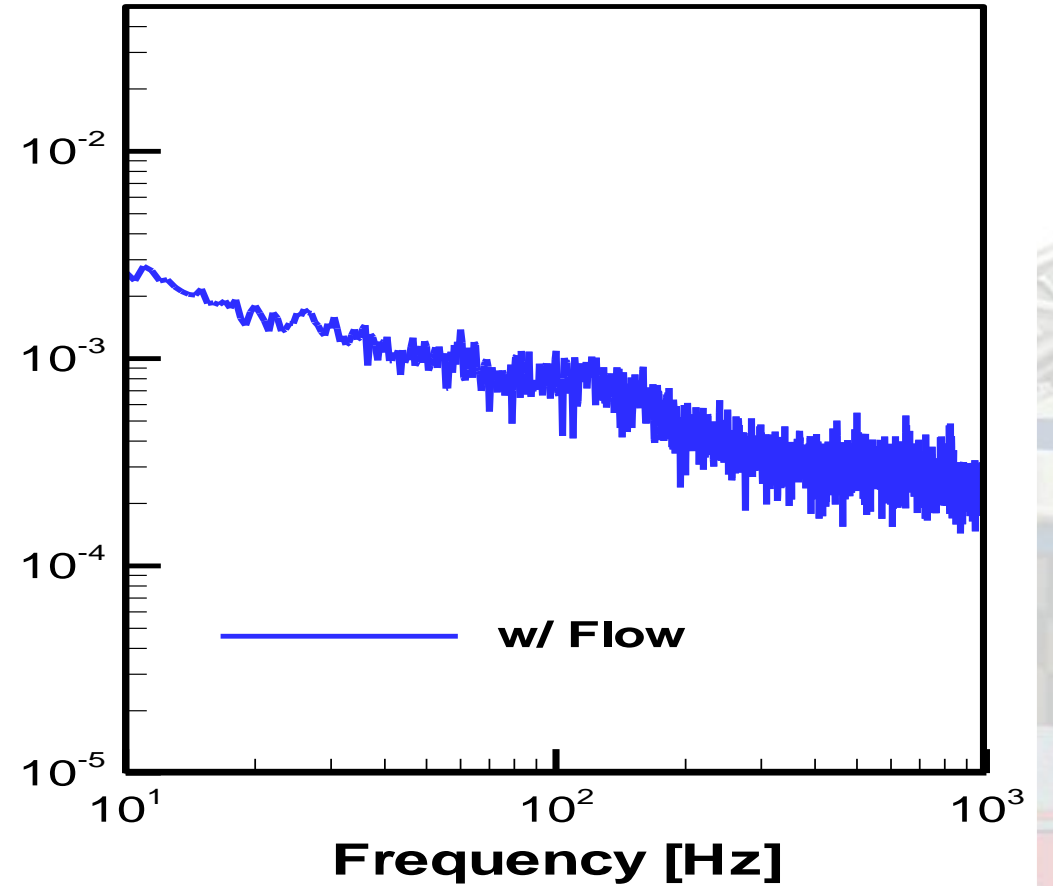
Thank you



Sensor selection



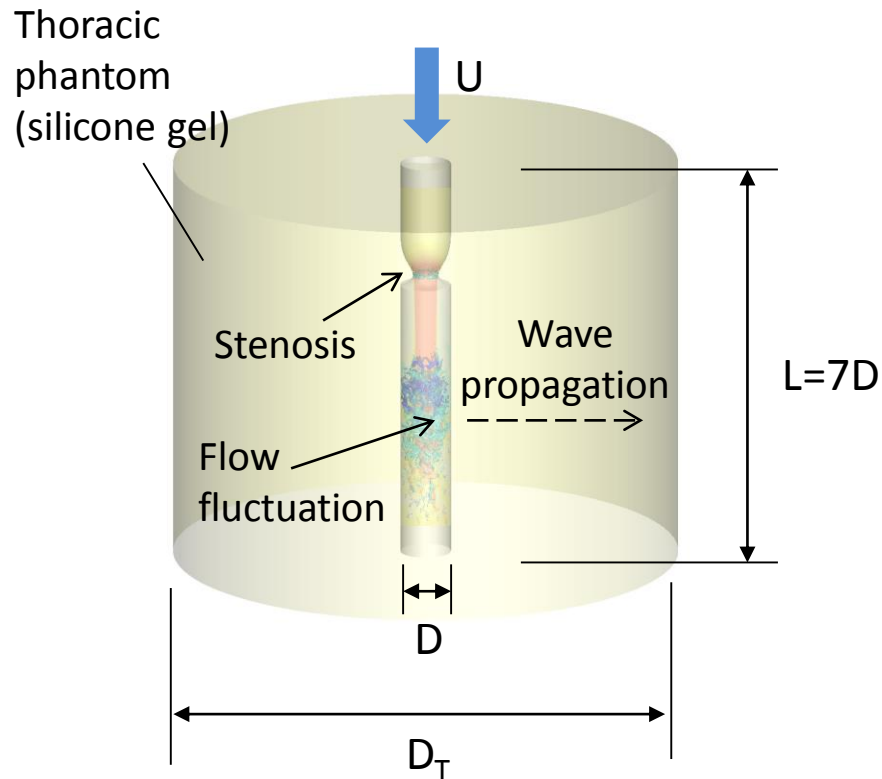
A: Electronic stethoscope



B: Accelerometers

Model for the Aortic Stenosis Murmur

For the joint computational/experimental study



$$Re = UD/\nu = 4000$$

$$St = fD/U$$

EcoFlex-10

$$\rho = 1040 \text{ kg/m}^3$$

$$K = 1.04 \text{ GPa} \quad (c_b = 1000.0 \text{ m/s})$$

$$G = 18.39 \text{ kPa} \quad (c_s = 4.2 \text{ m/s})$$

$$\mu = 14 \text{ Pa s}$$

$$U = 0.25 \text{ m/s}$$

$$D = 1.5875 \text{ cm}$$

$$D_T = 9.84 \text{ cm (gelA)}, 16.51 \text{ cm (gelB)}$$

c.f.

Biological soft tissue:

$$K = 2.25 \text{ GPa} \quad (c_b = 1500 \text{ m/s})$$

$$G = 0.1 \text{ MPa} \quad (c_s = 10 \text{ m/s})$$

$$\mu = 0.5 \text{ Pa s}$$

